

Temperature Stabilization in the receiver cabin of KVN antenna

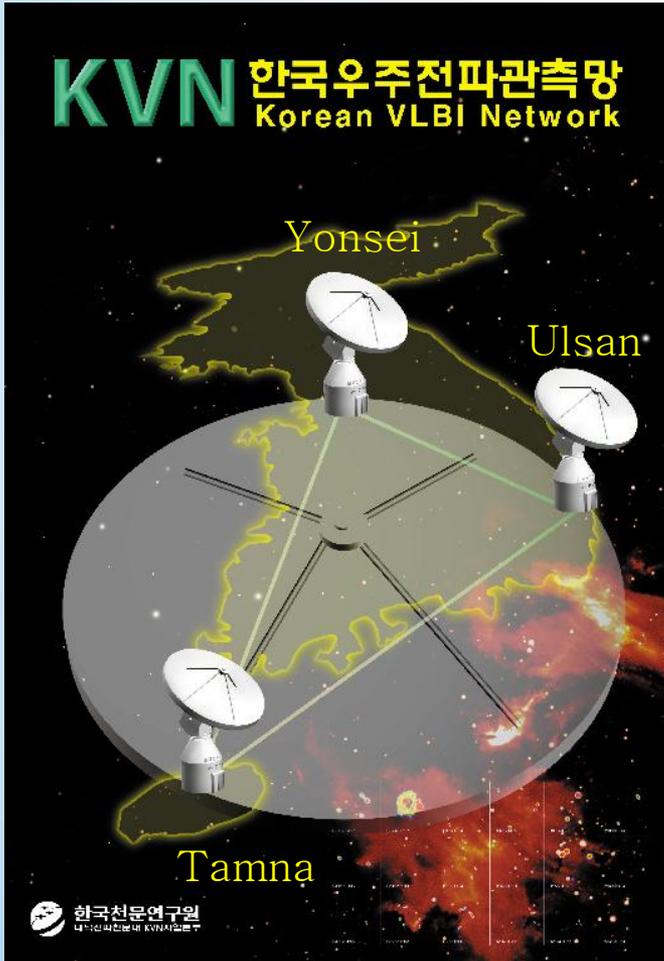
Seogoh, Wi (KASI KVN)

Nov. 24. 2015

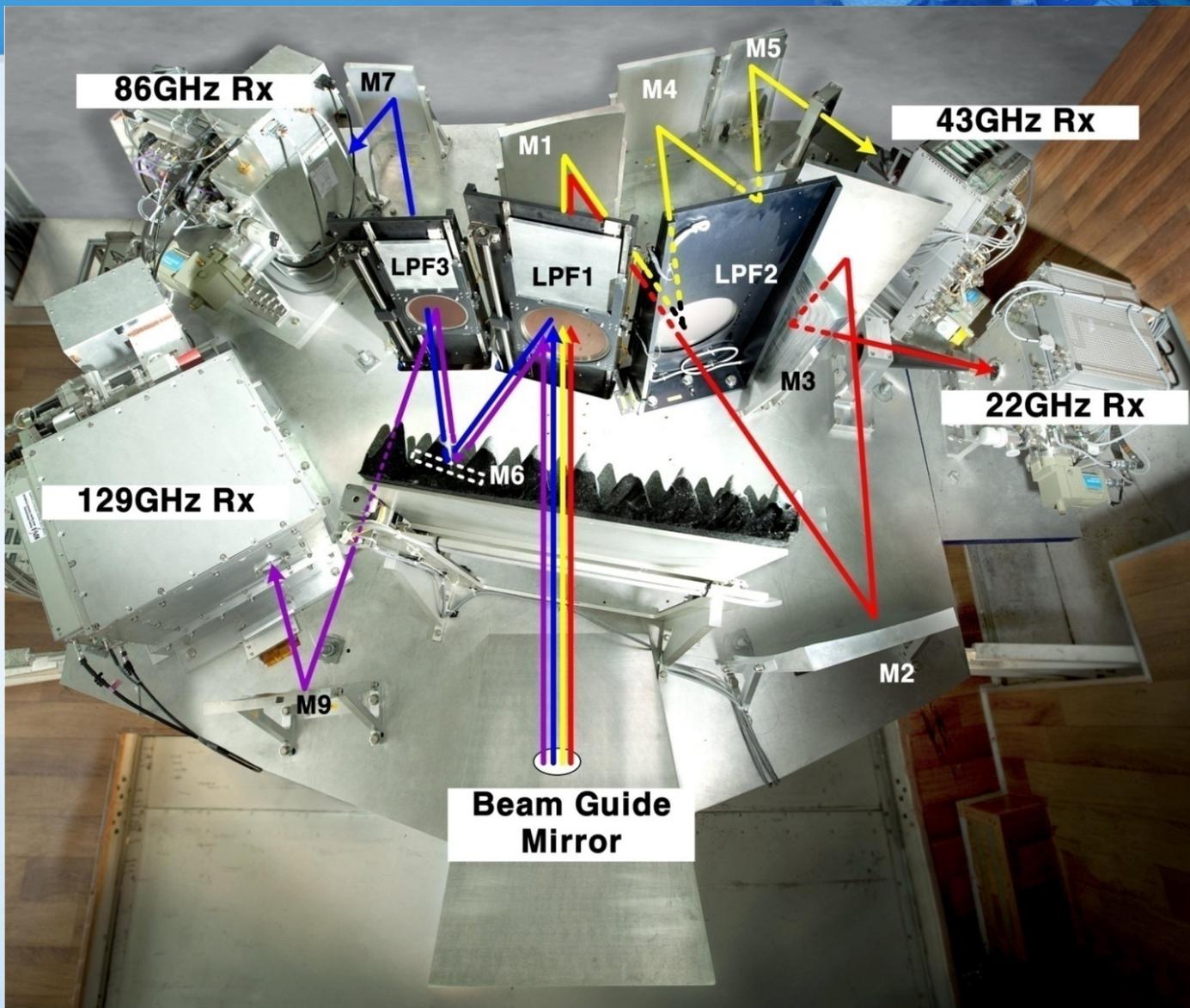
4th IVTW in Auckland, NZ



KVN 21m Radio Telescopes



KVN 4 channel Receiver



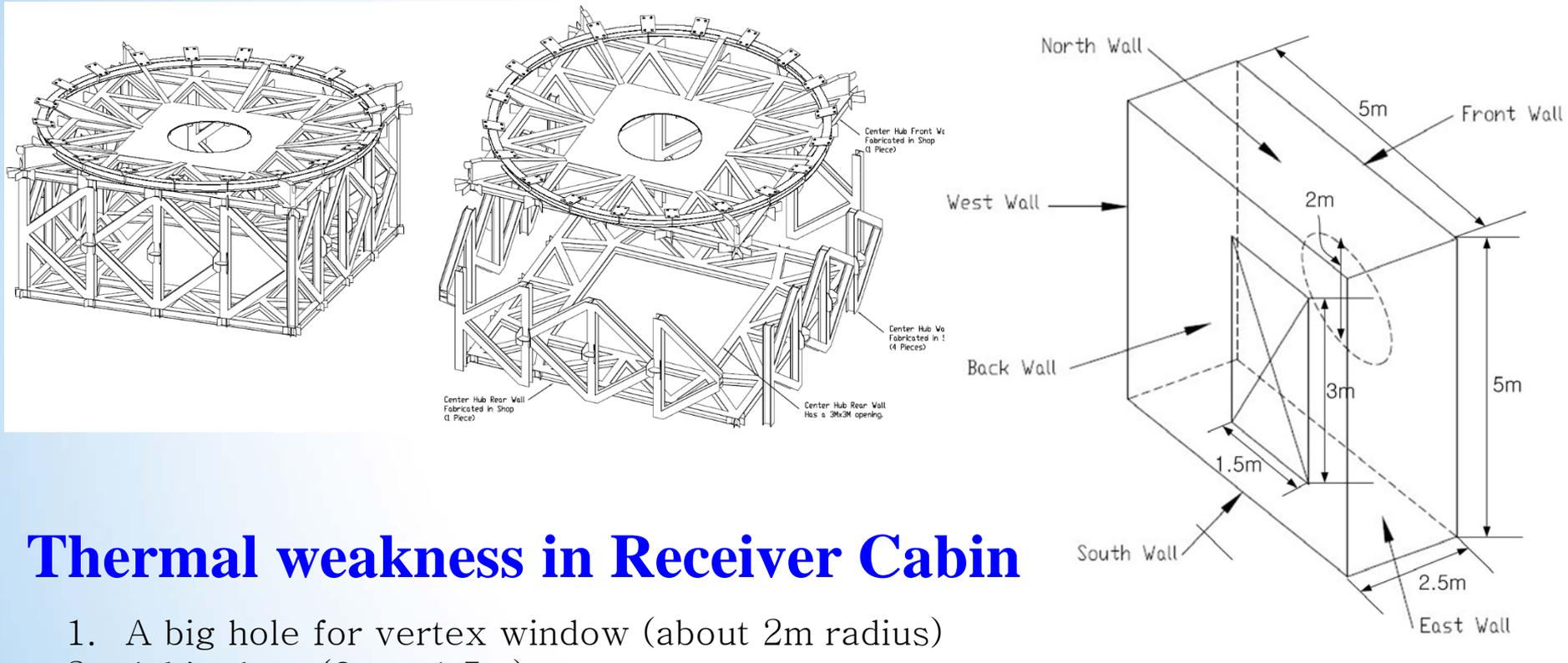
Phase stability in mm VLBI



- Atmospheric fluctuation
 - ✓ *4 channel receiver system*
- Instrumental phase noise due to ~
 - Cable length variation due to Mechanical vibration and temp.
 - ✓ *RTS : Phase stabilization from phase error due to cable length variation*
 - Characteristic change of Rx components due to **Temp. variation**
 - ✓ *Ultra wide band phase calibration (22GHz ~ 130GHz)*
 - Difficulties
 - ✓ **P-cal., RTS components itself,**
 - ✓ **cables after P-cal. or RTS**

*** Temperature stabilization in receiver cabin**
and H-maser room with new HVAC
within +/-0.5degC

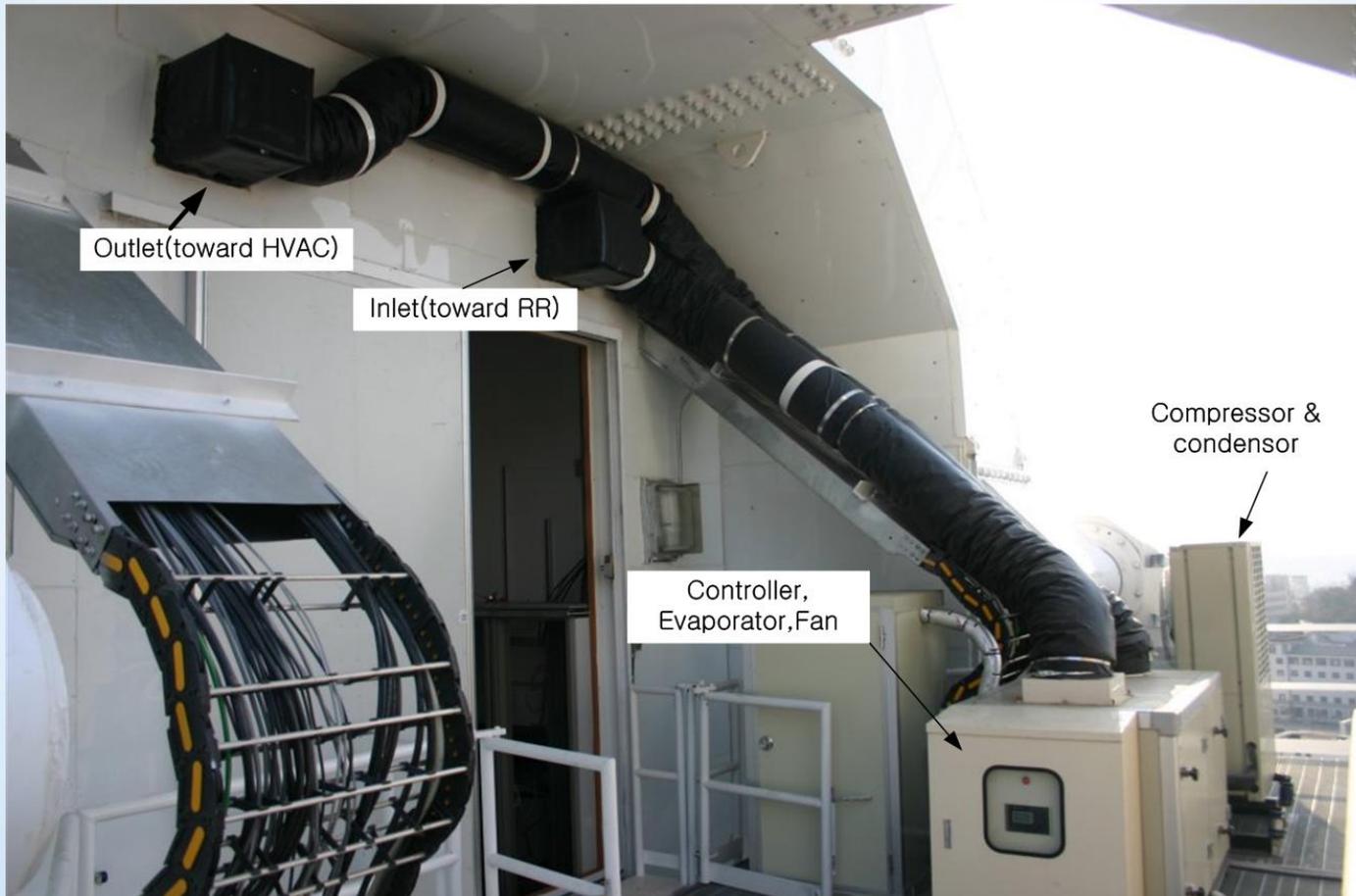
Structure of receiver cabin



Thermal weakness in Receiver Cabin

1. A big hole for vertex window (about 2m radius)
2. A big door (3m x 1.5m)
3. Two in/outlet holes for cables
4. Limitation of performance of insulation material
5. Thermal transmission through steel structure

Old Rx room HVAC

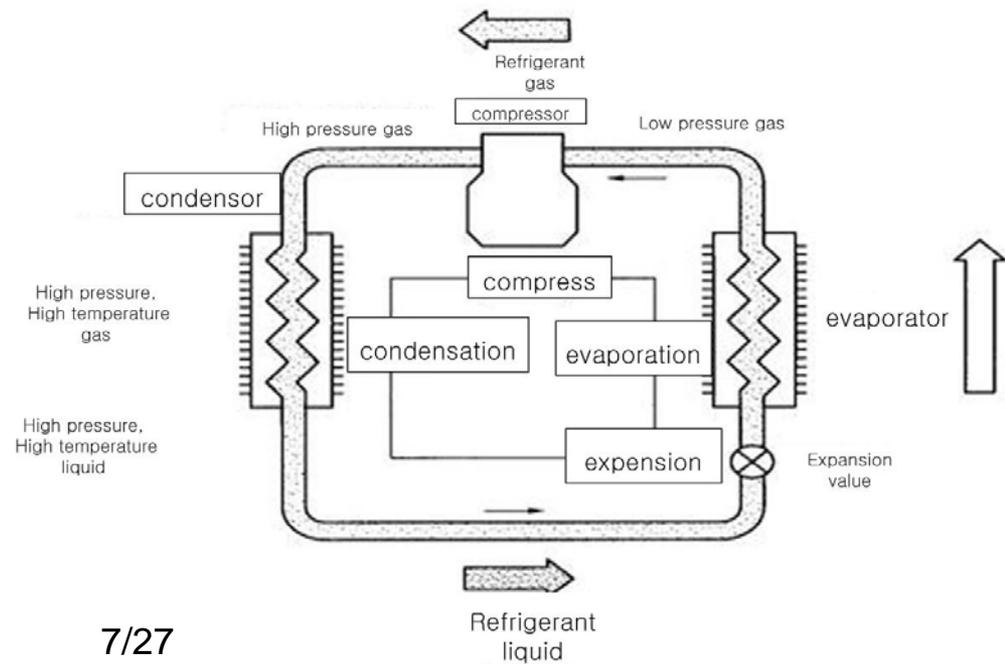
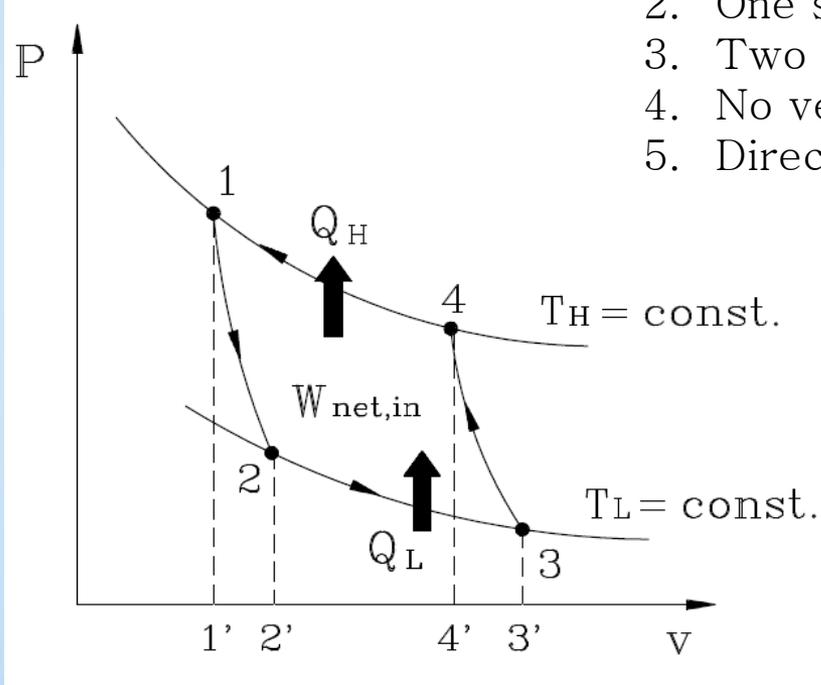


Conventional Refrigerator using reversal Carnot Cycle



Old Rx room HVAC

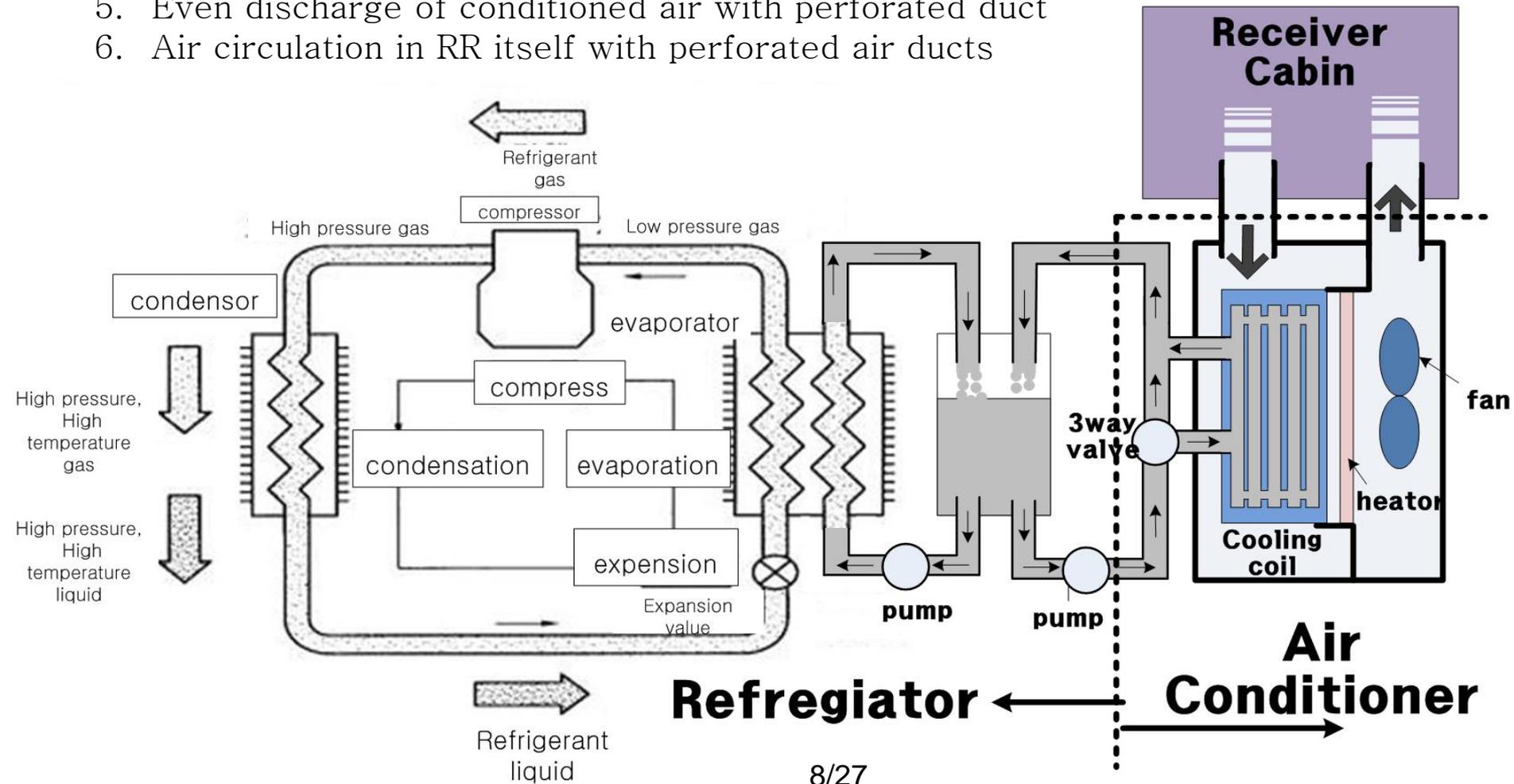
1. Temp. control range : ± 2 degC
2. One step refrigeration, On/Off control of compressor
3. Two step On/Off control of Heaters
4. No ventilation in receiver cabin in itself
5. Direct heat exchange at evaporator



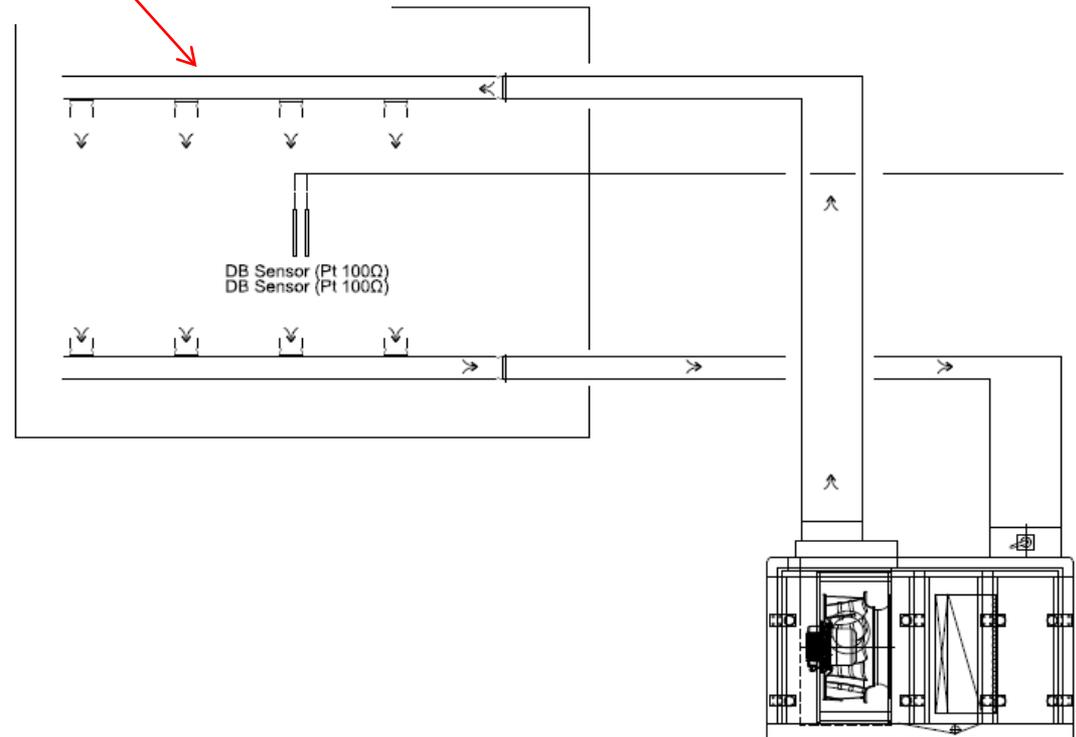
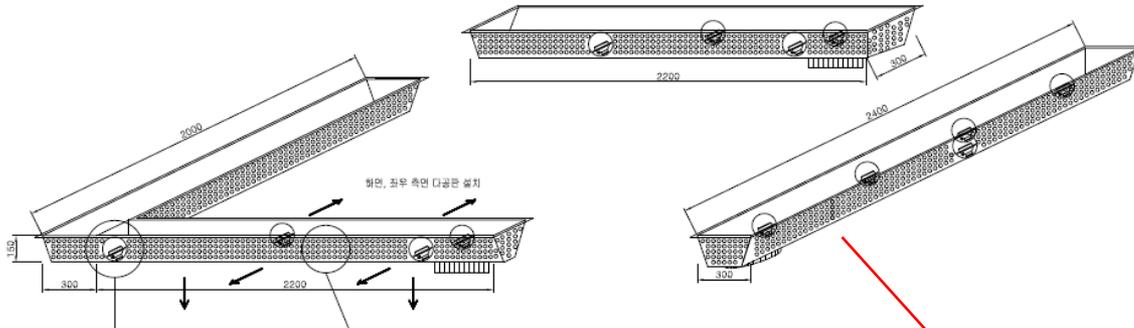
New Rx room HVAC



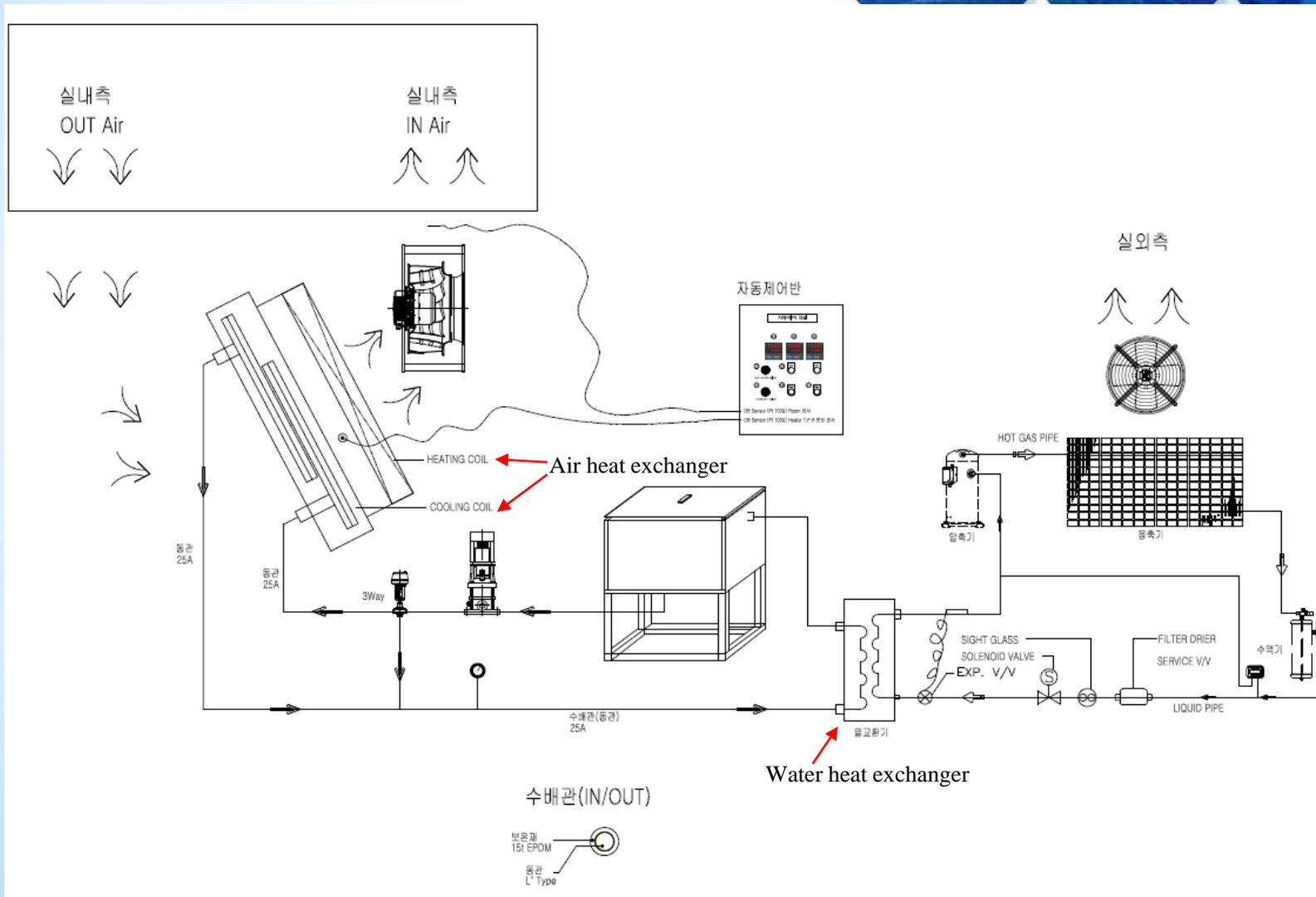
1. Temp. control range : ± 0.5 degC
2. Indirect heat exchanger at evaporator
3. PID control for 3 way water valve
4. PID control for heater
5. Even discharge of conditioned air with perforated duct
6. Air circulation in RR itself with perforated air ducts



Perforated ducts for Even discharge



Airflow diagram of new HVAC



Heat load (Total refrigeration capacity = heat load + control capacity) due to power load, radiation and convection



power load	load capacity(W)
Vacuum monitor	200
power supply for 22,43, 86 GHz Rx	500
conoller power for quasi optics	200
Total power detector	200
bias power for 129GHz Rx	500
monitor system for Rxs	300
Temp. monitor system	200
Base band converter	500
IF signal selector	500
frequency synthesizer	500
M&C computr for Rxs	500
Digital Sampler x 4ea	800
Digital signal optical transmitter	300
4channel receiver	1,000
lights and etc.	1,000
total	7,000

material	K	area [m ²]	air temp.	surface Temp. [k]	Temp. Diff. [k]	radiation rate	total radiation heat work rate [w]	natural convection coefficient	total convection heat work rate [w]
urethan	0.2	91.3	23	27	2	0.85	1,107	4.5	822
steel	4.3	1.1	23	27	2	0.85	13	4.5	10
styroform	0.6	0.8	23	38	15	0.85	76	4.5	53
aluminum	46.9	2.4	23	38	15	0.95	229	4.5	159
total							1,425		1,043

K : Thermal transmittency [W/m² · K]

Heat load from power usage
(heat from inside)

Heat load from radiation and convection
(heat from outside)

$$(7\text{kw} + 1.4\text{kw} + 1\text{kw}) \times 1.2 \text{ (reserve rate)} =$$

11.3kw

control capacity

to control air state from 38 °C(80% relative humidity) to 26 °C(60% relative humidity) within 15min



(1) 38°C(80% relative humidity) air enthalpy =

$$i_{38_80} = 0.24\text{cal/J} \times 38^\circ\text{C} + (597\text{kcal/kg} \\ + 0.441\text{kcal}/(\text{kg}^\circ\text{C}) \times 38^\circ\text{C}) \times 0.03\text{kg} = 27.53\text{kcal/kg}$$

(2) 23°C(60% relative humidity) air enthalpy =

$$i_{23_60} = 0.24\text{cal/J} \times 23^\circ\text{C} + (597\text{kcal/kg} \\ + 0.441\text{kcal}/(\text{kg}^\circ\text{C}) \times 23^\circ\text{C}) \times 0.015\text{kg} = 14.62\text{kcal/kg}$$

(3) Difference of enthalpy = $i_{38_80} - i_{23_60} = 12.9\text{kcal/kg} = 53\text{kJ/kg}$

(4) **Control capacity** : Refrigeration capacity to control air state from 38 °C(80% relative humidity) to 26 °C (60% relative humidity) within 15min

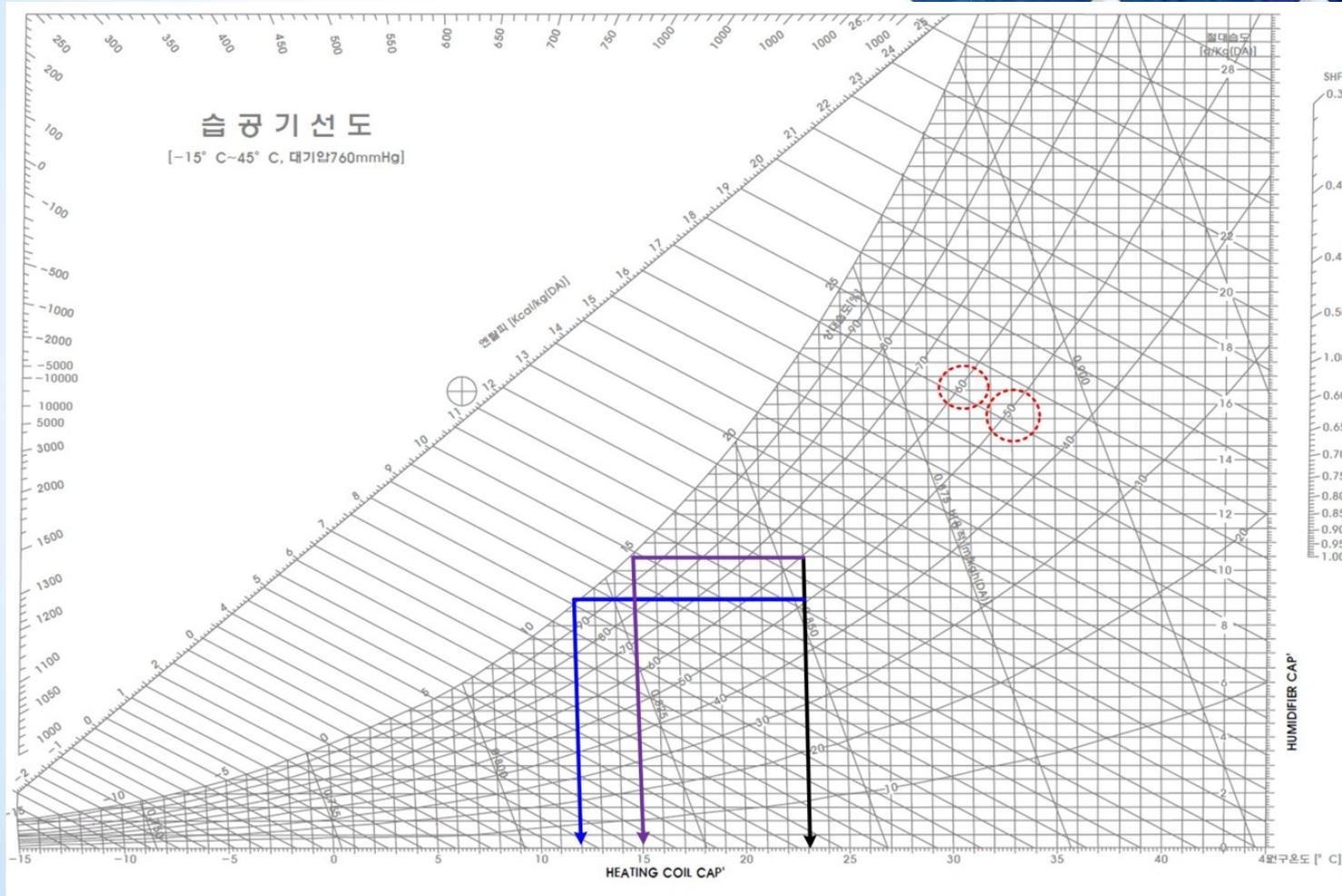
$$1.2\text{kg/m}^3 \times 100\text{m}^3 \times 53\text{kJ/kg} = 6,360\text{kJ} \rightarrow 6,360\text{kJ}/15\text{min} = 7.06\text{kJ/s} = 7.06\text{kw}$$

Total refrigeration capacity = heat load + control capacity

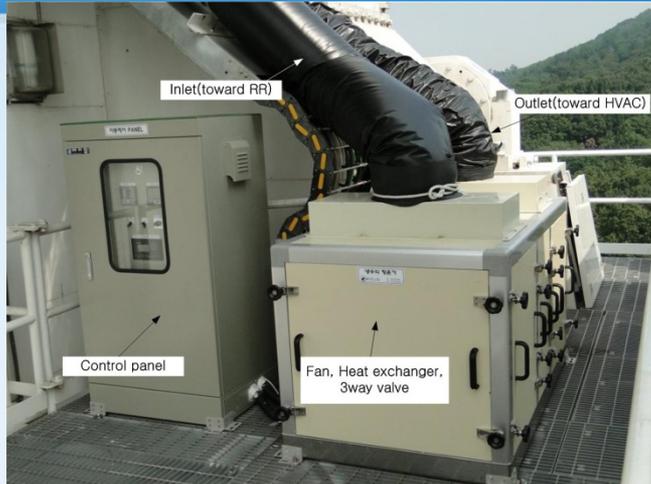
$$= 11.3\text{kw} + 7.06\text{kw} = 18.36\text{kw} = 18.36\text{kw} \times \text{IRT}/4\text{kw} = \sim 5\text{RT}$$

Psychrometric chart for KVN HVAC

(temp: 23degC, Humidity control < 60% : water < 15degC)



New Rx room HVAC system



Air heat exchanger and air blower



Compressor, condenser and water heat exchanger



Perforated air duct in receiver cabin



Distribution box for air ducts

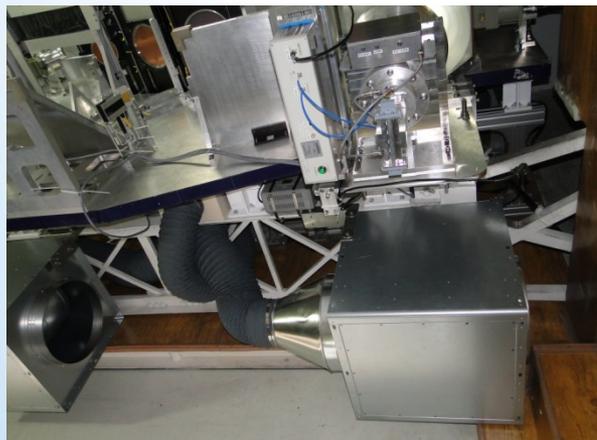
Ideas for air circulation and ventilation



Air distribution box in RR for air discharge



Inlet box for even air suction in receiver cabin

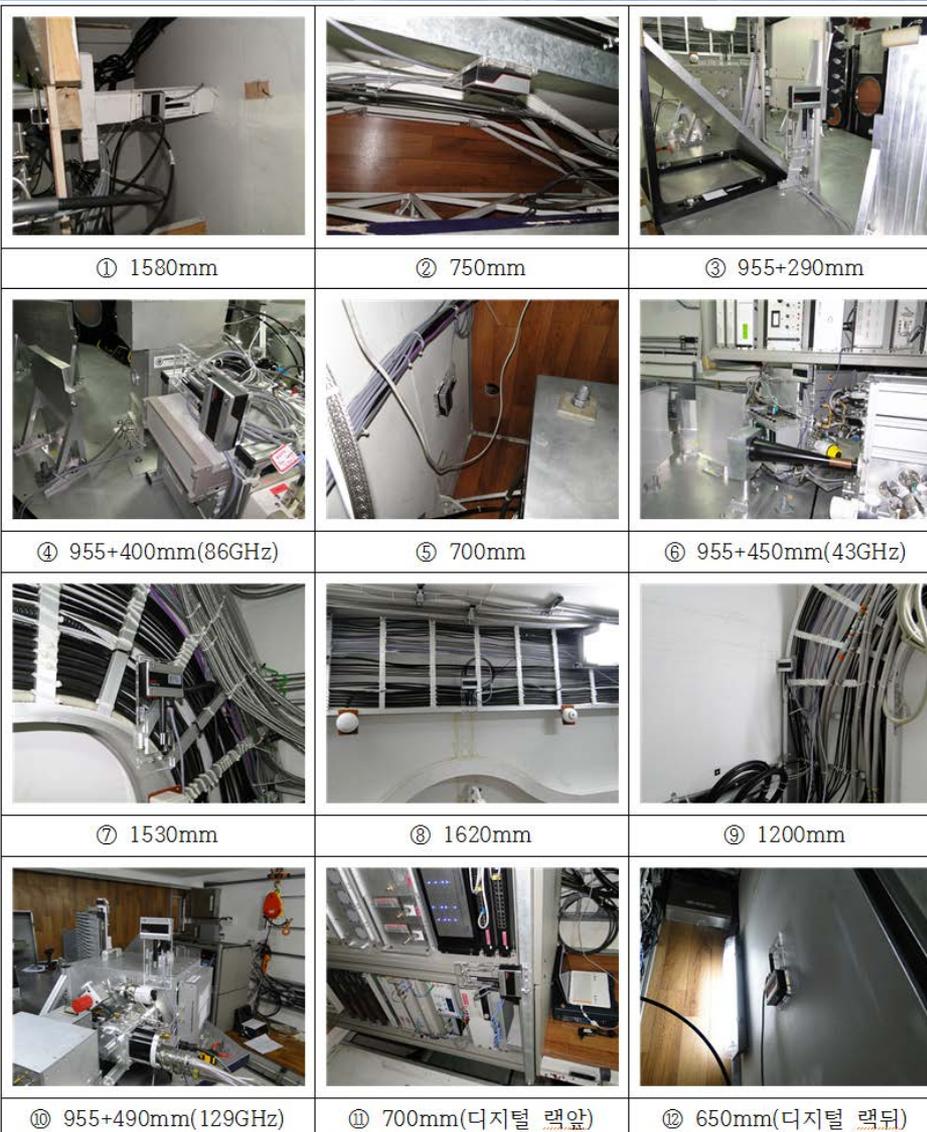


Blowers in RR air circulation in receiver cabin

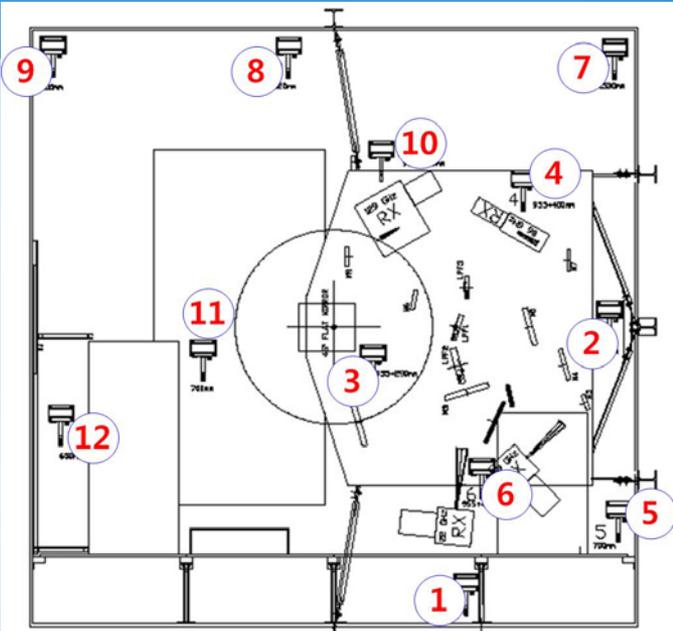


Perforated air ducts for air circulation

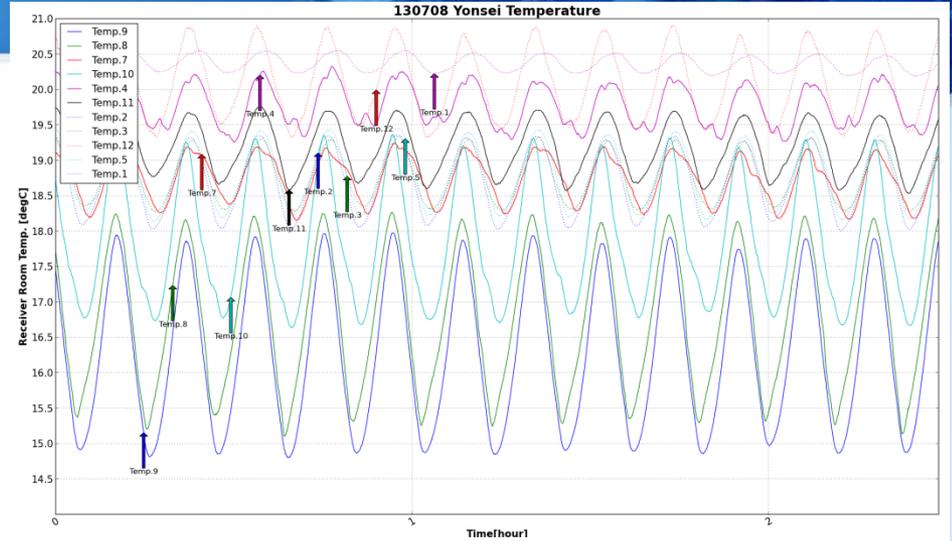
Temperature sensors in receiver cabin



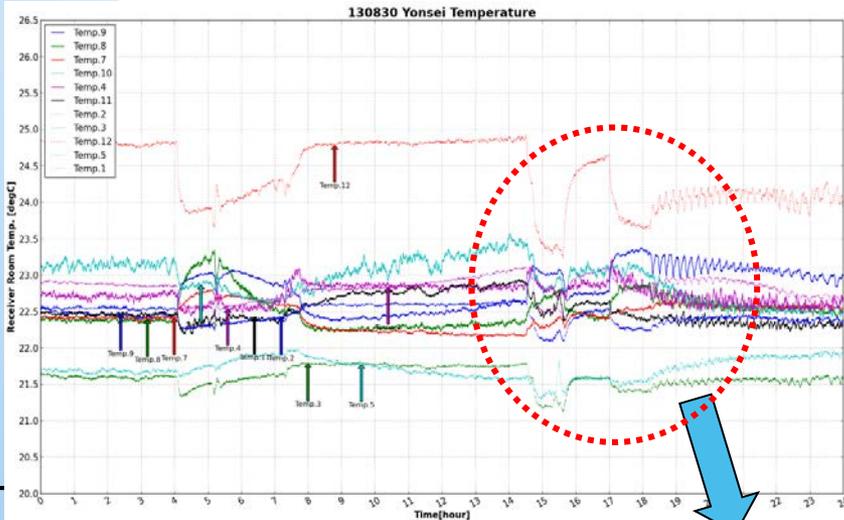
Monitoring Temp. in RR



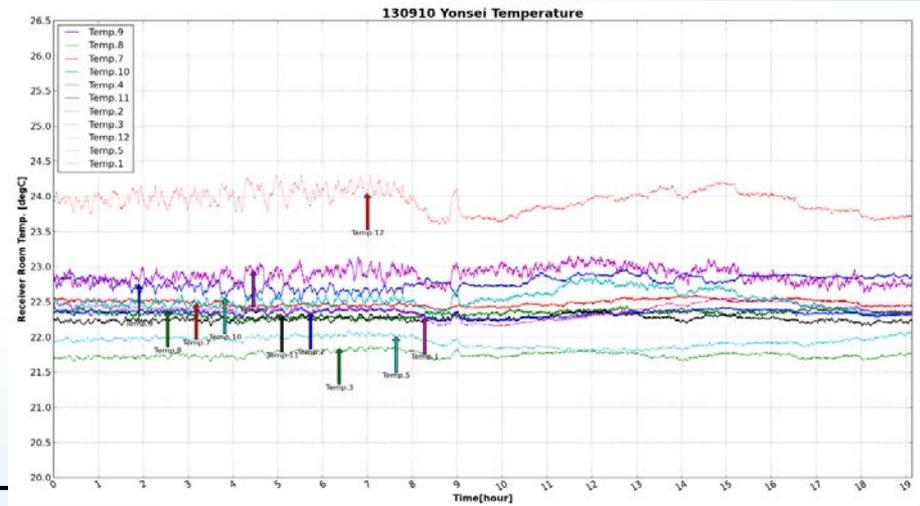
Position of Temp. sensors in receiver room



Temperature in RR with old HVAC (stow position)

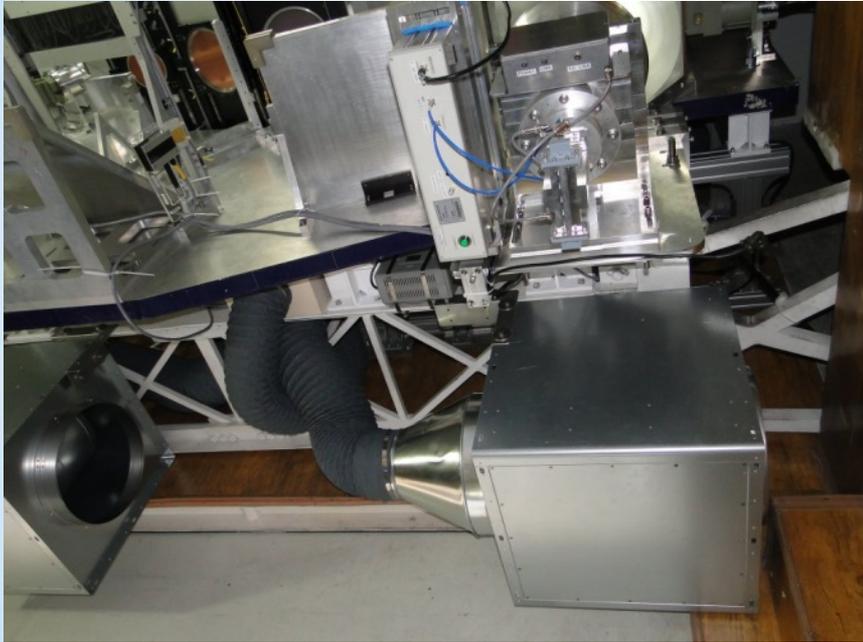


Temperature in RR with new HVAC (stow position) Before air circulation 17/27

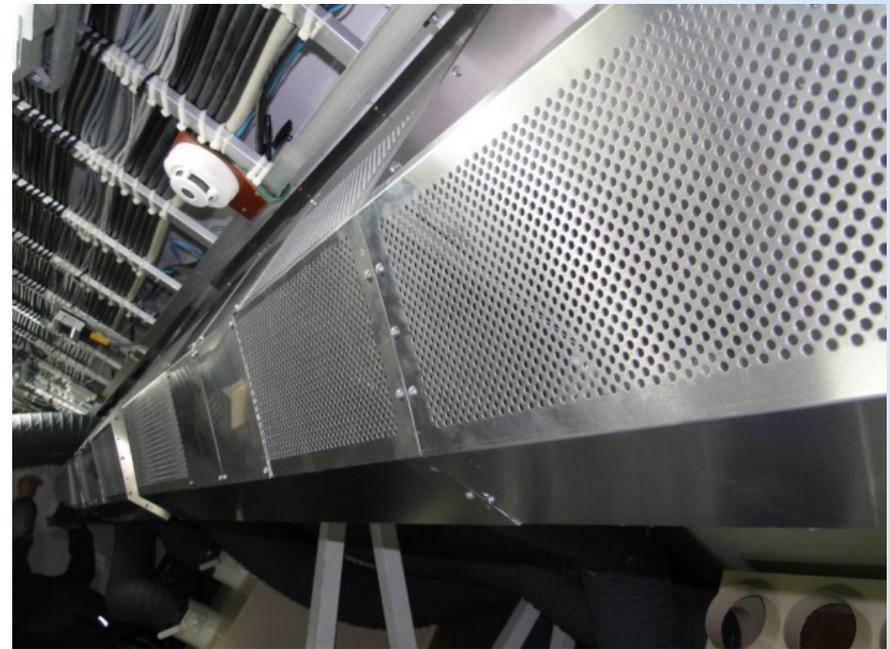


Temperature in RR with new HVAC (stow position)

Air circulation with blower and ducts

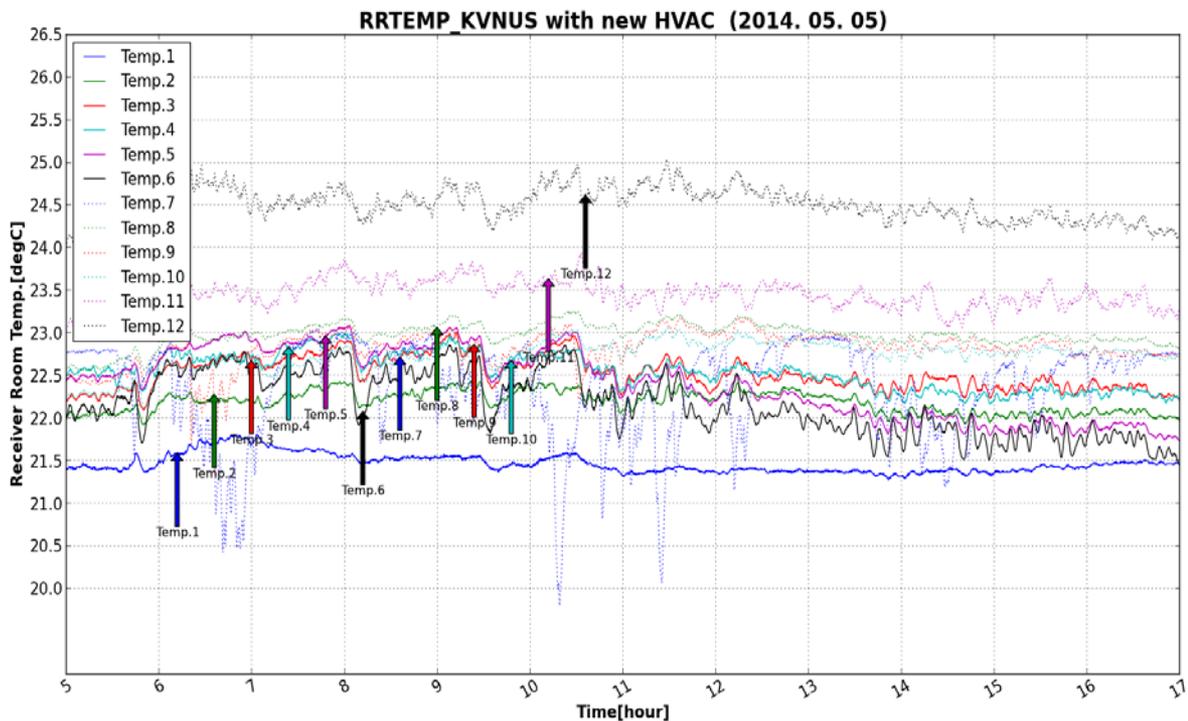


Blowers in RR air circulation in receiver cabin

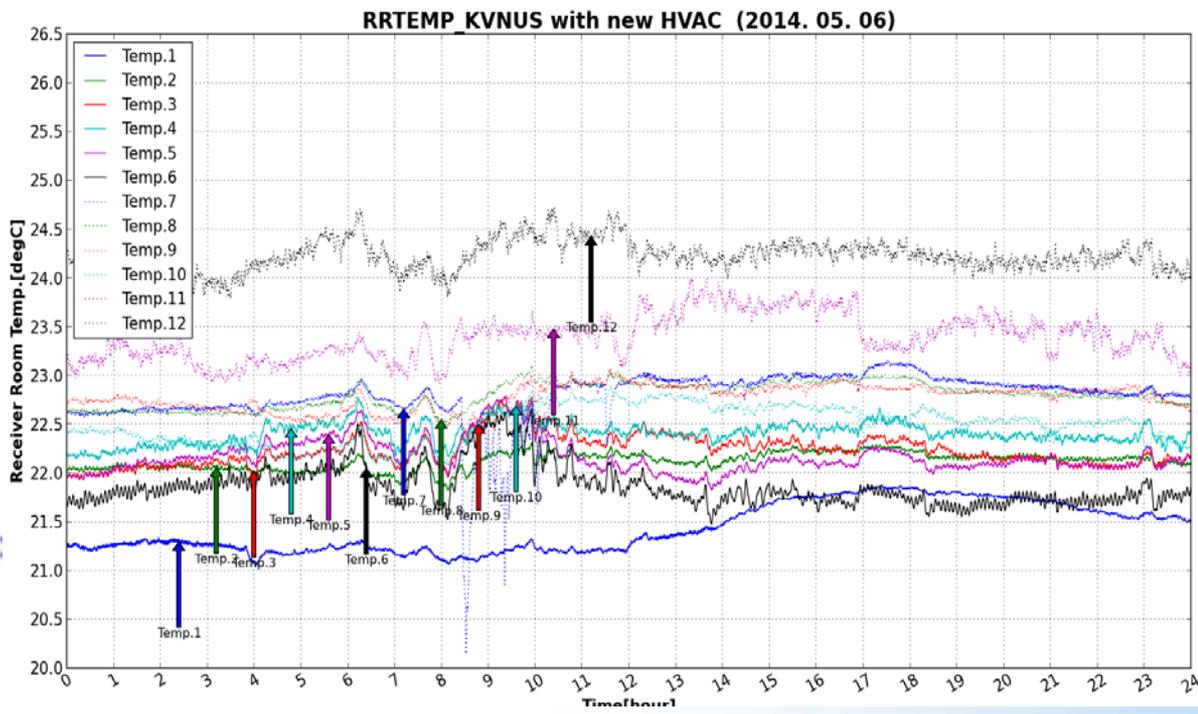


Perforated air ducts for air circulation

Ulsan receiver room Temp. w/ new HVAC and Vent.



Ulsan receiver room Temp. w/ new HVAC and Vent.



Yonsei H-maser room HVAC



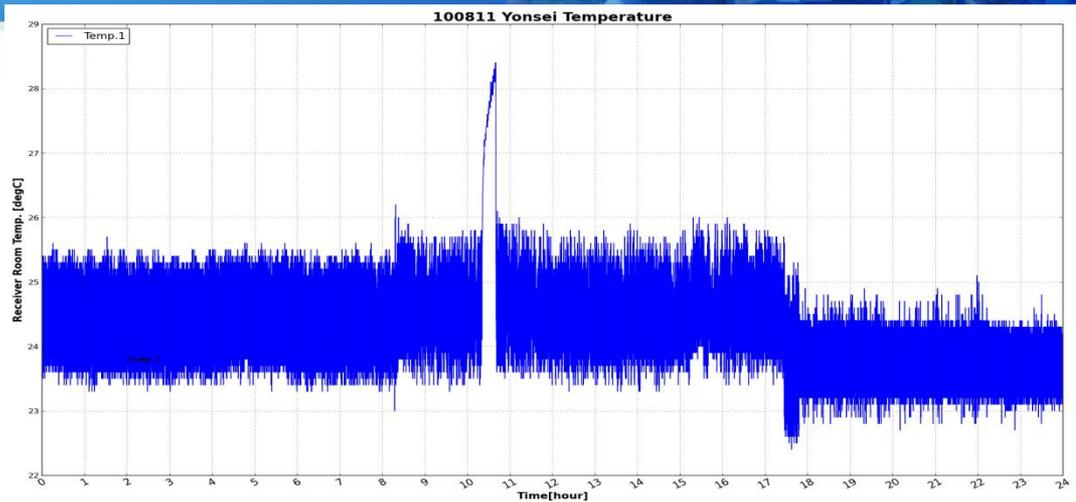
수소시계실 HVAC 공조기, 제어기



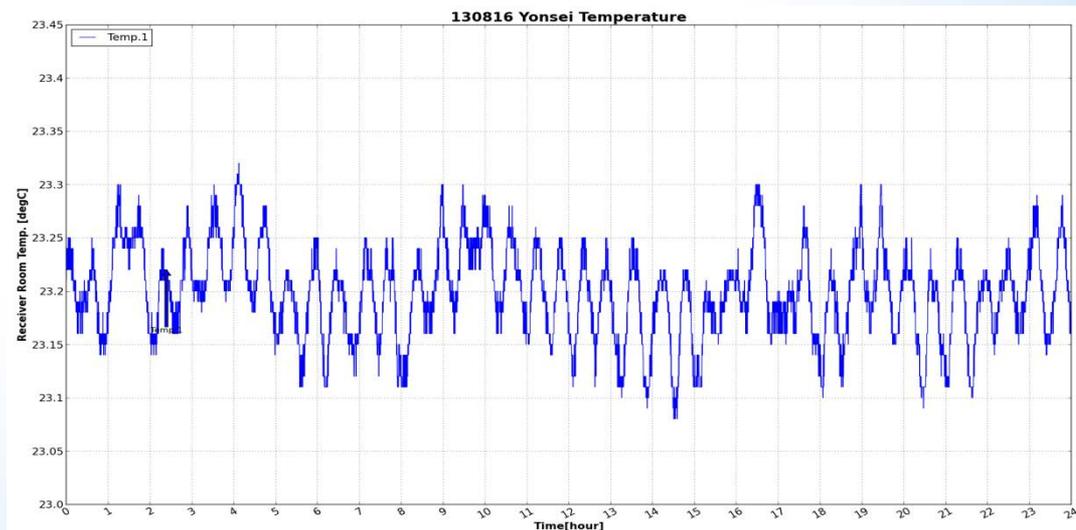
수소시계실 다공판 토출덕트



수소시계실 용 냉수식 컴프레서

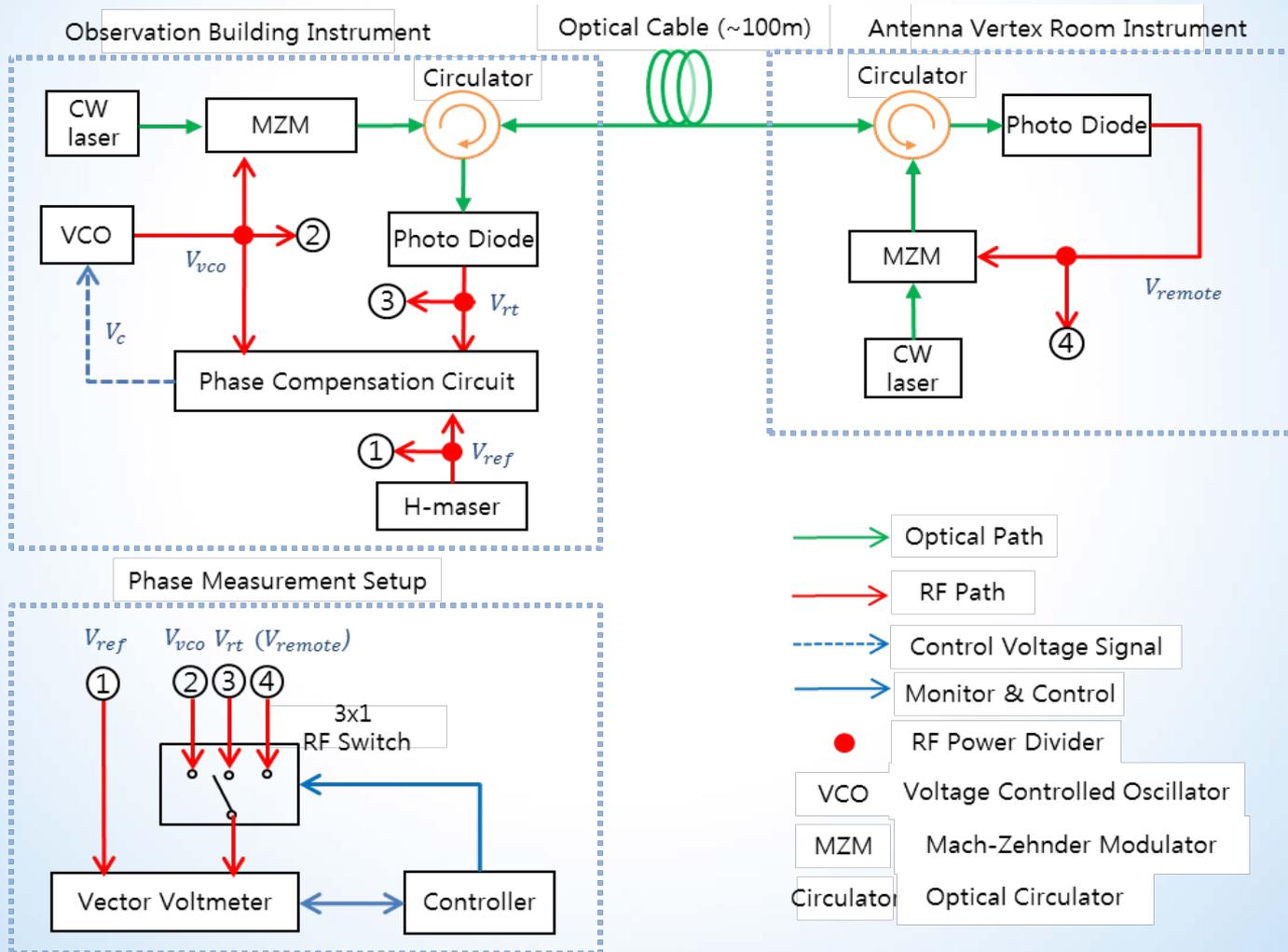


수소시계실내 온도 (old HVAC → +1.5degC)

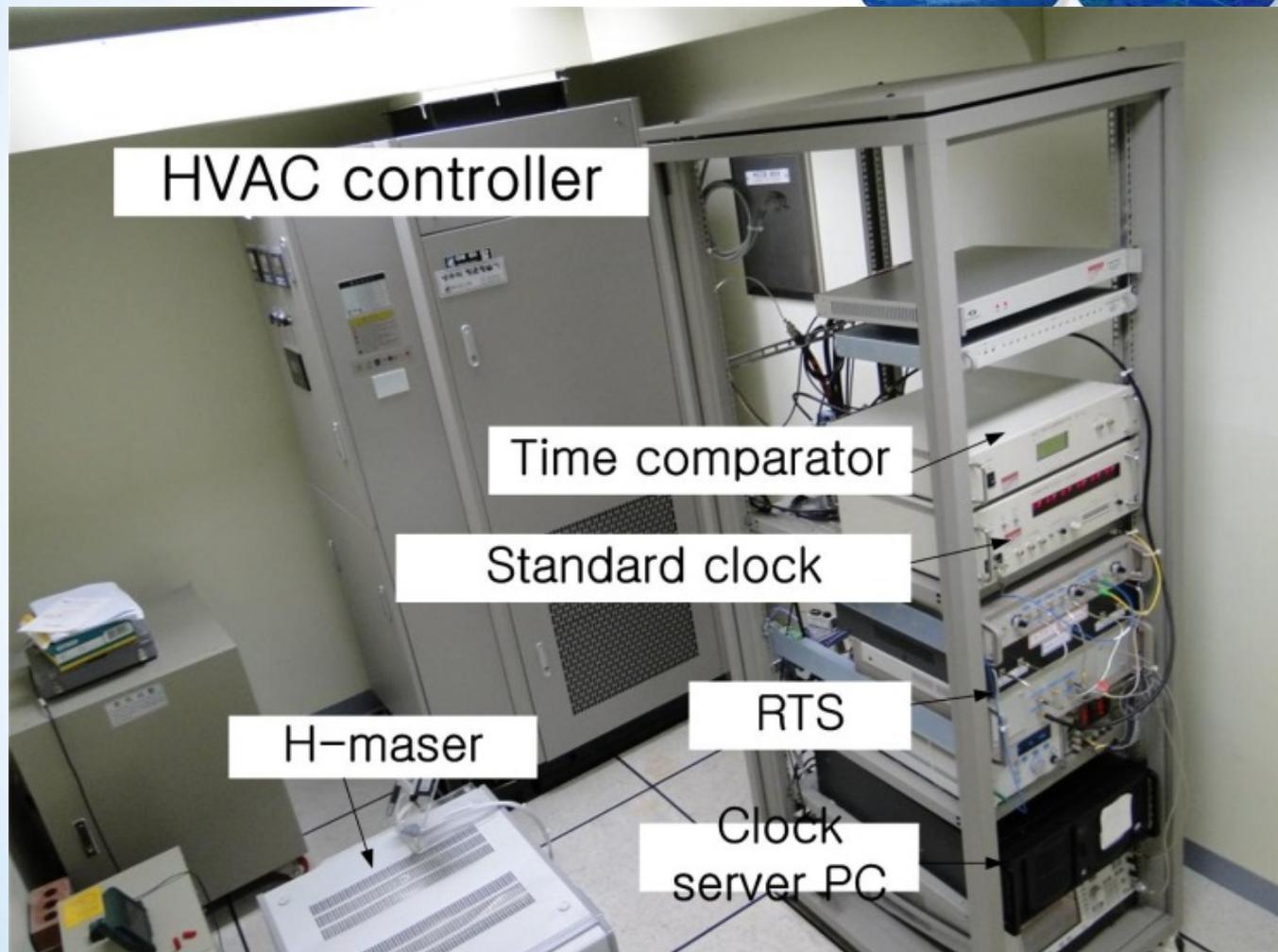


수소시계실내 온도 (new HVAC → +0.1degC)

Round Trip Monitor system for phase noise monitoring



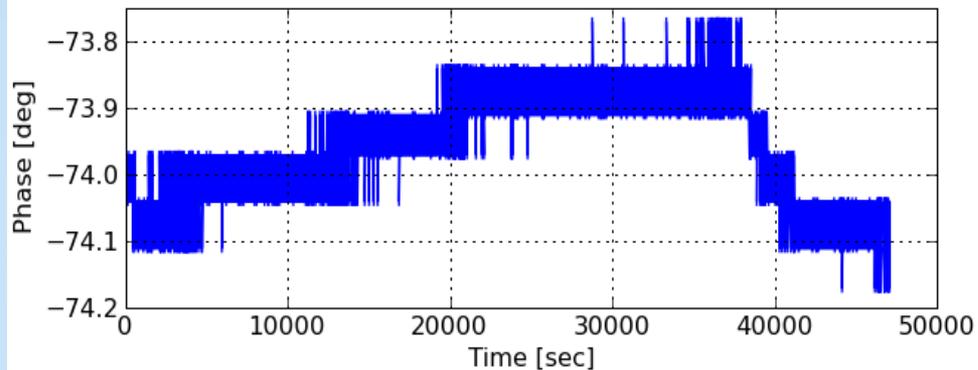
Installation of clock related instruments in H-maser room after temperature stabiiization



Temp., phase variation with old HVAC

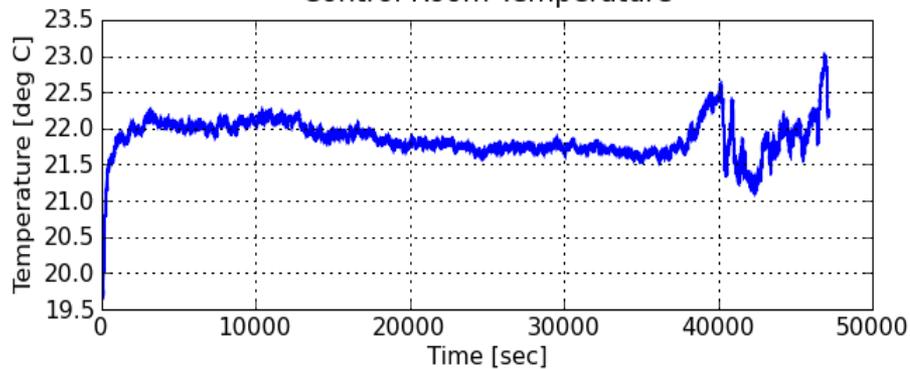


Phase B-A (Remote-Ref)



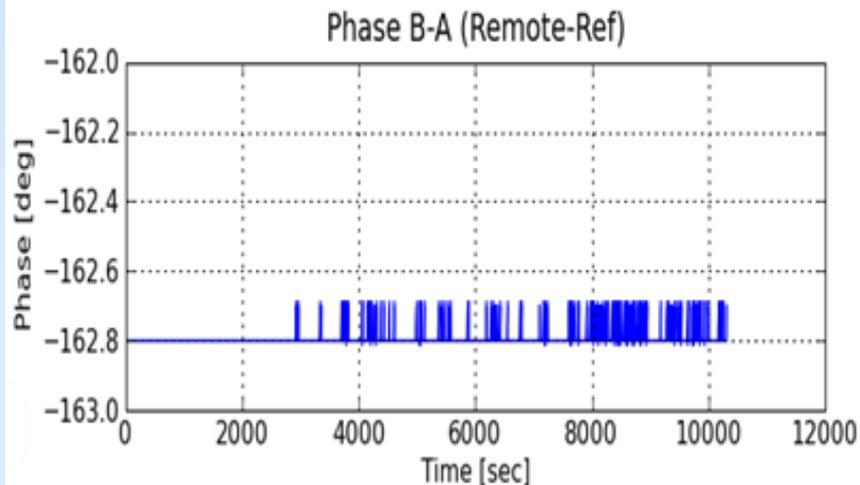
Phase difference b/w H-maser and RR reference signal : $< 0.4\text{deg}$ @ 1.4GHz)

Control Room Temperature

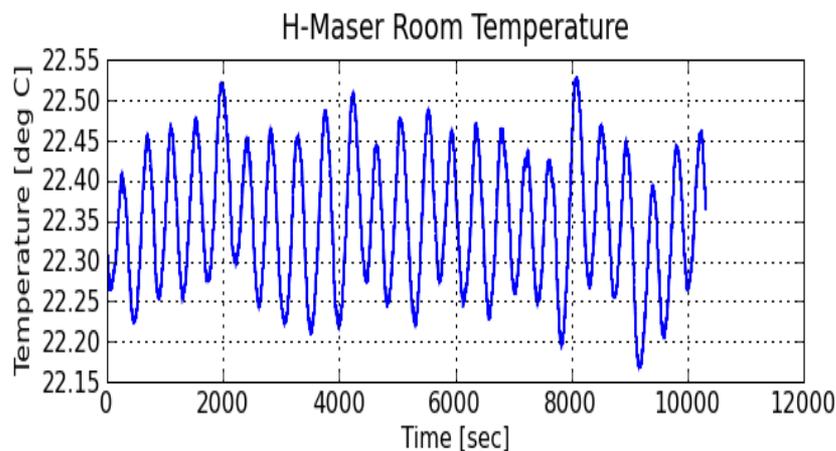


Temperature variation at H-maser : $< \pm 2\text{degC}$

Temp., phase variation with new HVAC

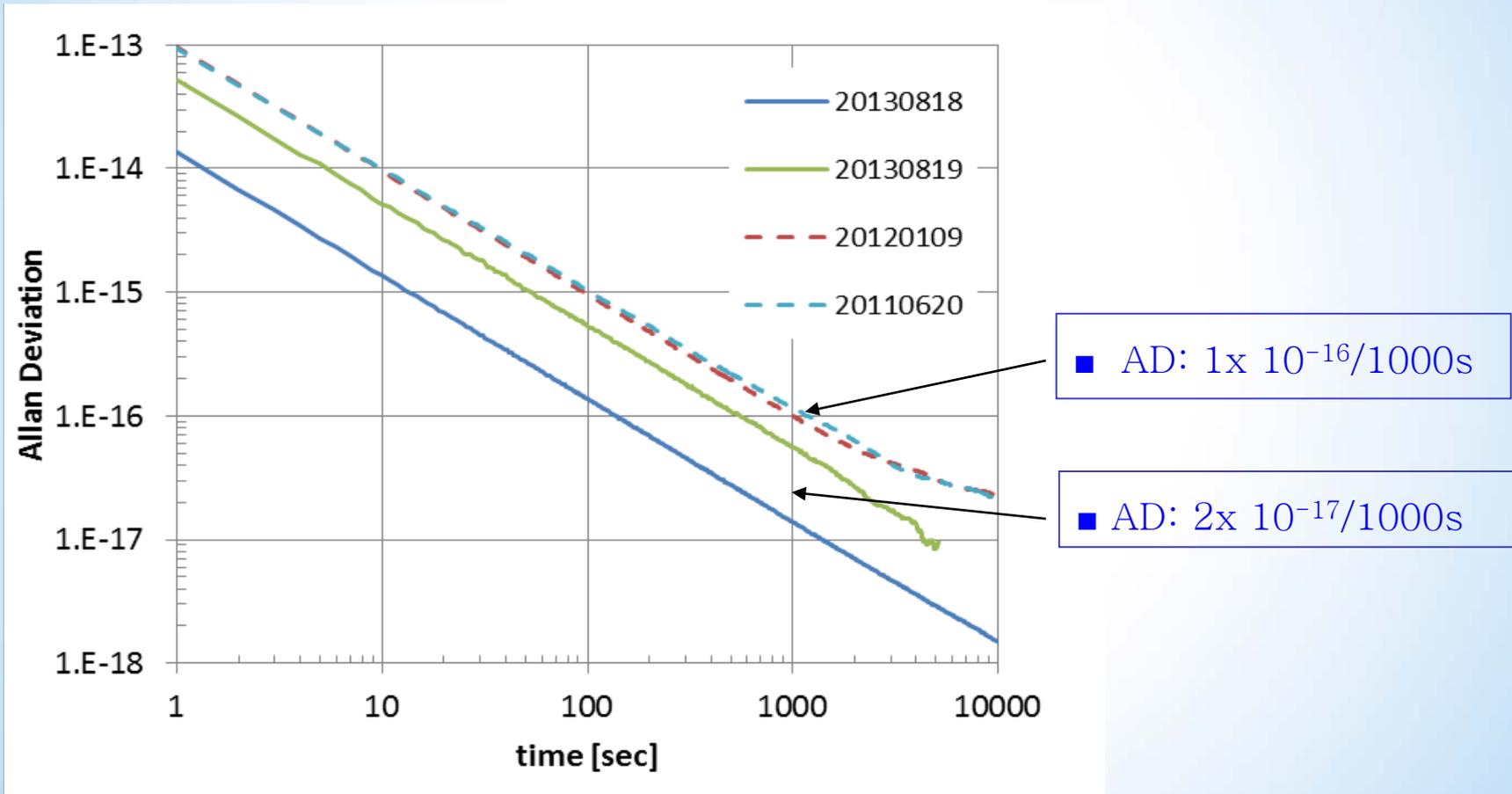


Phase difference b/w H-maser and RR reference signal : $< 0.1 \text{deg}$ @ 1.4GHz)



Temperature variation at H-maser : $< \pm 0.1 \text{degC}$

Alan deviations for phase noise



Alan deviations of phase noise is improved twice.

Summary



- Indirect heat exchanging with water as intermediate material
- PID controller of three way water valve to stabilize temp. of cooling coil (water)
- PID controller of heater for stabilization of final air temperature
- Perforated duct, duct distribution box for in/outlet
- Perforated ducts and blower for air circulation
- Temperature sensor and monitor
- New HVAC for receiver cabin: $< + - 0.5\text{degC/per channel (24h operation)}$
- New HVAC for H-maser room: $< + - 0.1\text{degC/per channel (24h operation)}$
- Relative humidity ratio : $< 60\%$
- Phase stabilization of RTS : Allen deviation : $1 \times 10^{-16}/1000\text{s} \rightarrow 2 \times 10^{-17}/1000\text{s}$



Thank you for your attention